

# \* Columns \*

\* Ground Floor height = 5 m

\* Typical Floor height = 3 m

\*  $F_{cu} = 250 \text{ Kg/cm}^2$

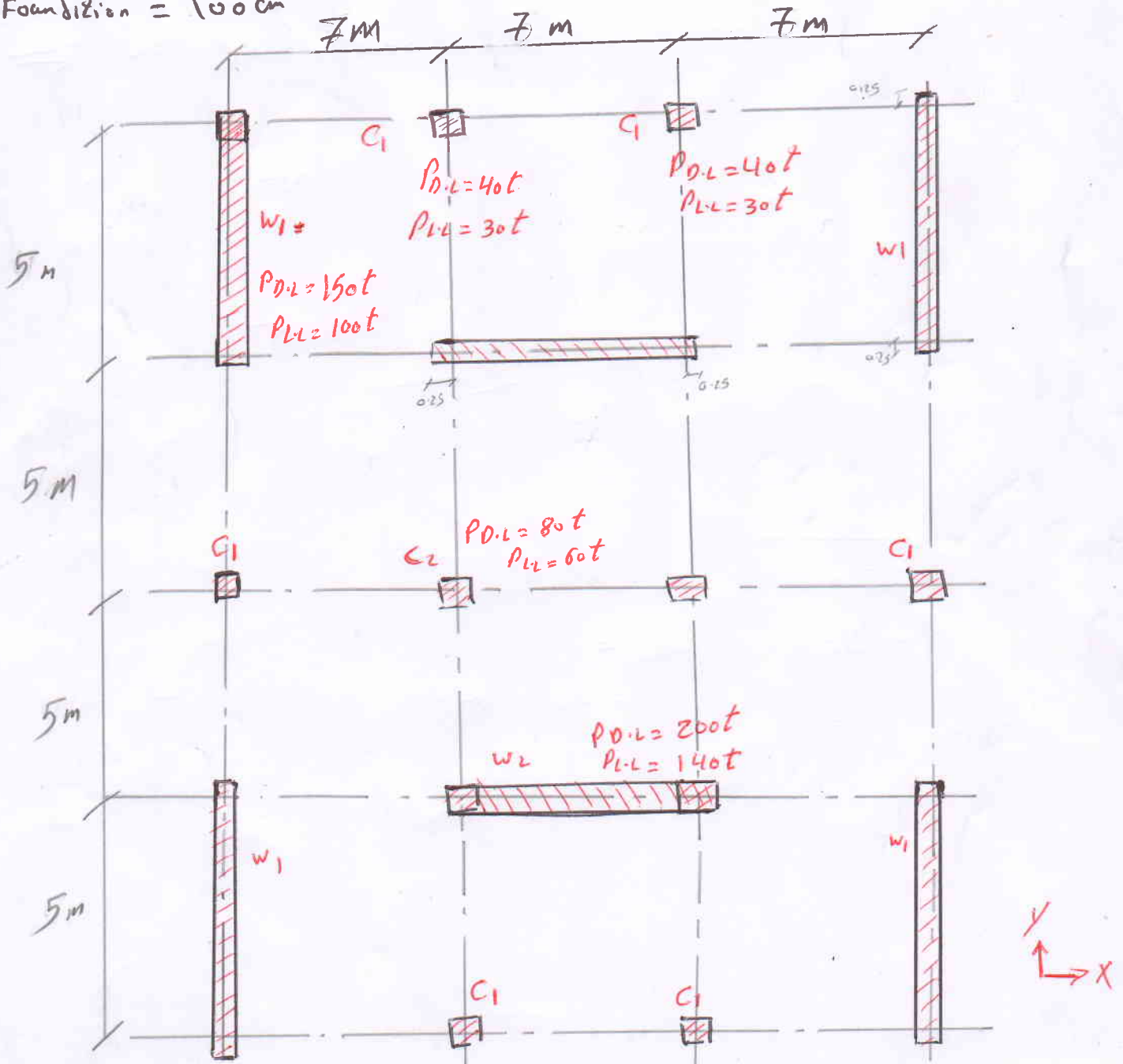
\*  $F_y = 3600 \text{ Kg/cm}^2$

\*  $n = 7 \text{ Floor}$

\* all thicknesses walls = 30 cm

\*  $t_{\text{Floor}} = 25 \text{ cm}$

\*  $t_{\text{Foundation}} = 100 \text{ cm}$



$$\Rightarrow \alpha = H \sqrt{\frac{N}{\sum EI}} \leq 0.5 \quad n \geq 4$$

$$\alpha = H \sqrt{\frac{N}{\sum EI}} \leq (0.2 + 0.1n) \quad n < 4$$

$$\therefore H = 5 + 0.3 = 23 \text{ m}$$

$$E_c = 14000 \sqrt{F_c} = 14000 \sqrt{250} = 221359.44 \text{ Kg/cm}^2 \\ = 2213594.4 \text{ t/m}^2$$

$N = \text{working loads}$

$$N = 4W_1 + 2W_2 + 6C_1 + 2C_2$$

$$N = [4(150 + 100) + 2(200 + 140) + 6(40 + 30) + 2(80 + 60)] * 7$$

$$N = 16660 \text{ t}$$

$\Rightarrow y$  direction

$$\alpha_y = H \sqrt{\frac{N}{\sum EI_x}}$$

$$I_{x_{w_1}} = \frac{0.3 * (5.5)^3}{12} * 4 = 16.637 \text{ m}^4$$

$$\alpha_y = 23 \sqrt{\frac{16660}{16.637 * 2213594.4}} = 0.489 < 0.6$$

The Building is Braced in y direction

⇒ X direction:

$$\alpha_x = H \sqrt{\frac{N}{\sum EI_x}}$$

$$I_y = \frac{0.3 * (7.5)^3}{12} * 2 = 21.09 \text{ m}^4$$

$$\alpha_x = 23 \sqrt{\frac{18880}{21.09 * 2213594.4}} = 0.43 < 0.6$$

The Building is Braced in X direction

\* Design C<sub>1</sub>:

$$P_u = [1.4(40) + 1.6(30)] * 7 * 1.1$$

$$P_u = 800.8 \text{ t}$$

$$P_u = 0.35 F_u A_c + 0.87 A_s F_y$$

$$\text{Assume } A_s = 1\% A_c$$

$$800.8 * 10^3 = 0.35 * 250 * A_c + 0.87 * \frac{1}{100} * A_c * 3600$$

$$A_c = \frac{800.8 * 10^3}{111.62} = 7174.34$$

$$A_c = t^2 \Rightarrow t = 84.7 \approx 85 \text{ cm}$$

(Column (85 x 85))

To get  $t(K)$

\* Case A :

Fixed  $\Rightarrow t_b > t_c$  or  $t_b > b_c$  and Foundation when designed to carry moment

\* Case B :

Partially Fixed  $t_b < t_c$

\* Case C :

hinged



\* Case D :

Free end

(unable to prevent Rotation  $\rightarrow$  slabs)

$\Rightarrow$  at X & Y direction

(check slenderness)

$$t = 0.85 \text{ m}$$

$$H_0 = 4.75 \text{ m}$$

lower end  $\rightarrow$  A

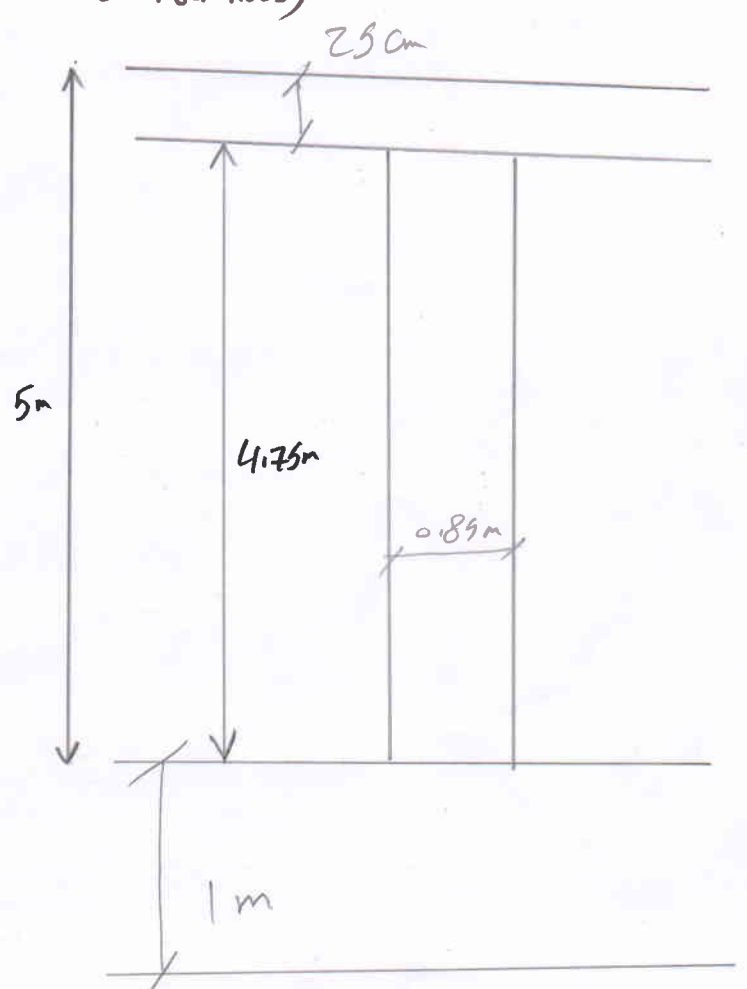
upper end  $\rightarrow$  B

$$K = 0.8$$

$$H_e = K H_0$$

$$= 0.8 * 4.75 = 3.8 \text{ m}$$

$$\lambda = \frac{H_e}{t} = \frac{3.8}{0.85} = 4.47$$

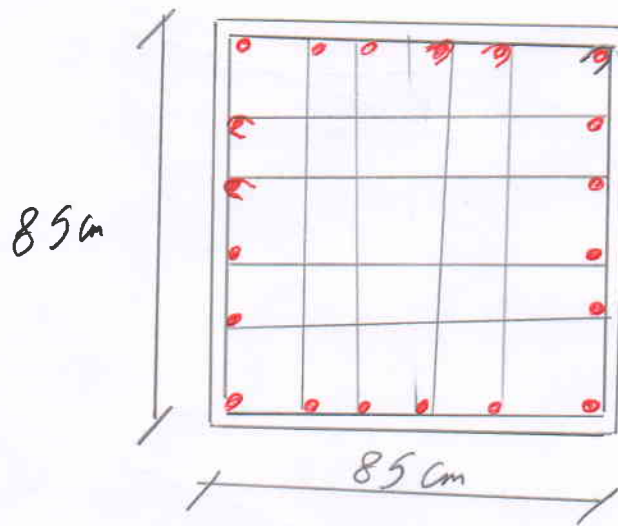


The column is short in both direction

$$A_s = 1\% A_c = \frac{1}{100} (85 \times 85)$$

$$A_s = 72.25 \text{ cm}^2$$

Take 20  $\phi$  22



\* Check stirrups:

$$\frac{V_s}{V_c} > 0.25\%$$

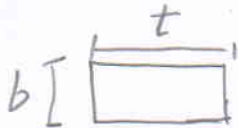
\* Example:

Braced building in Two direction

$$b = 25 \text{ cm}, \quad F_{cu} = 250 \text{ Kg/cm}^2$$

$$F_y = 3600 \text{ Kg/cm}^2, \quad p_u = 290 \text{ t}$$

Solution:



$$p_u = 0.35 F_{cu} A_c + 0.67 F_y A_s$$

$$A_s = 1\% A_c$$

$$290 \times 10^3 = A_c \left[ 0.35 \times 250 + \frac{1}{100} \times 0.67 \times 3600 \right]$$

$$A_c = 2598.1 \text{ cm}^2 = b \times t$$

$$t = \frac{A_c}{b} \approx 105 \text{ cm}$$

⇒ In plan Building:

$$t = 105 \text{ cm}$$

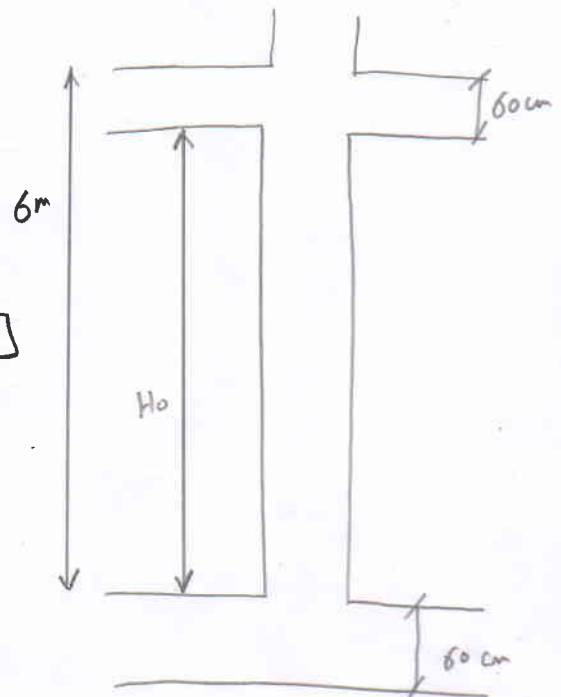
$$H_0 = 6 - 0.6 = 5.4 \text{ m}$$

$$H_e = K \times H_0$$

$$K = 0.85$$

$$H_e = 0.85 \times 5.4 = 4.59 \text{ m}$$

$$\lambda = H_e / t = \frac{4.59}{1.05} = 4.37 < 15 \text{ Short Column}$$



Upper  $t_b < t_c$   
Case B

Lower  $t_b < t_c$   
Case B

\* out of Plan Buckling :

$$b = 25 \text{ cm}$$

upper  $t_b > t_c$

$$H_0 = 5.4$$

$$K = 0.75$$

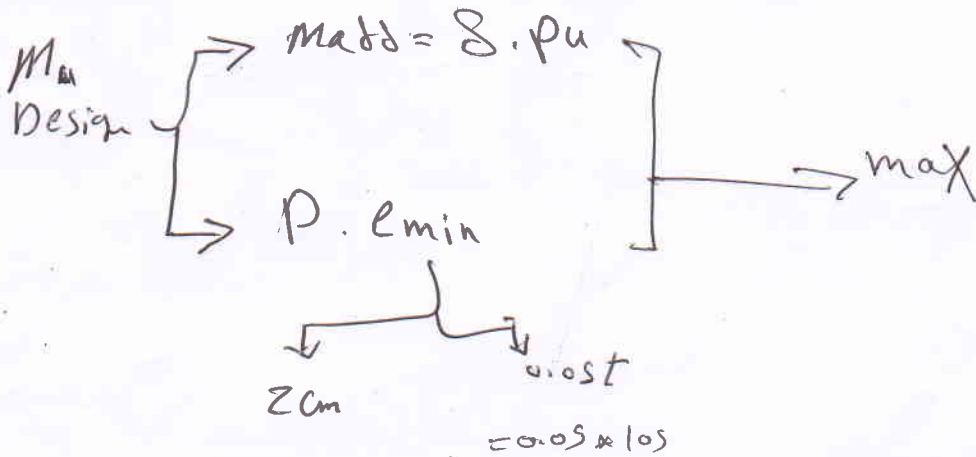
lower  $t_b > t_c$

$$H_e = 0.75 \times 5.4 = 4.05 \text{ m}$$

$$\lambda_b = \frac{H_e}{b} = \frac{4.05}{0.25} = 16.2 > 5$$

Long column

⇒ Design column As Long column



$$M_u = \left[ \begin{aligned} M_{add} &= \frac{I_b^2 \cdot k}{2000} \cdot P_u = \frac{16.2^2 \cdot 0.25}{2000} \cdot 290 \\ &= 9.513 \text{ t.m} \\ P \cdot e_{min} &= 290 \cdot 0.052 = 15.225 \end{aligned} \right] \rightarrow 15.225$$

$$M_{Design} = 15.225 \text{ t.m}$$

⇒ Use The Interaction Diagram:

$$K = \frac{P_u}{F_u \cdot b \cdot t} = \frac{290 \times 10^3}{250 \times 25 \times 105} = 0.441$$

$$K \cdot e/t = \frac{M_u}{F_u \cdot b \cdot t^2} = \frac{15.225 \times 10^3}{250 \times 25 \times (105)^2} = 0.022$$

$$\gamma = \frac{t - z_{cover}}{t} = \frac{105 - 5}{105} = 0.95$$

$$F_y = 3600 \text{ kg/cm}^2$$

⇒ use uniformly Distributed Steel

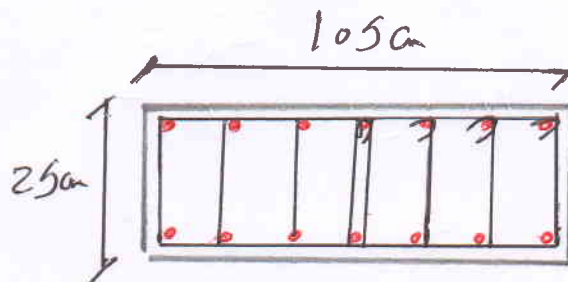
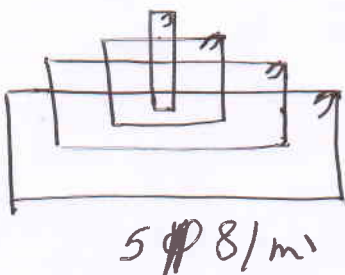
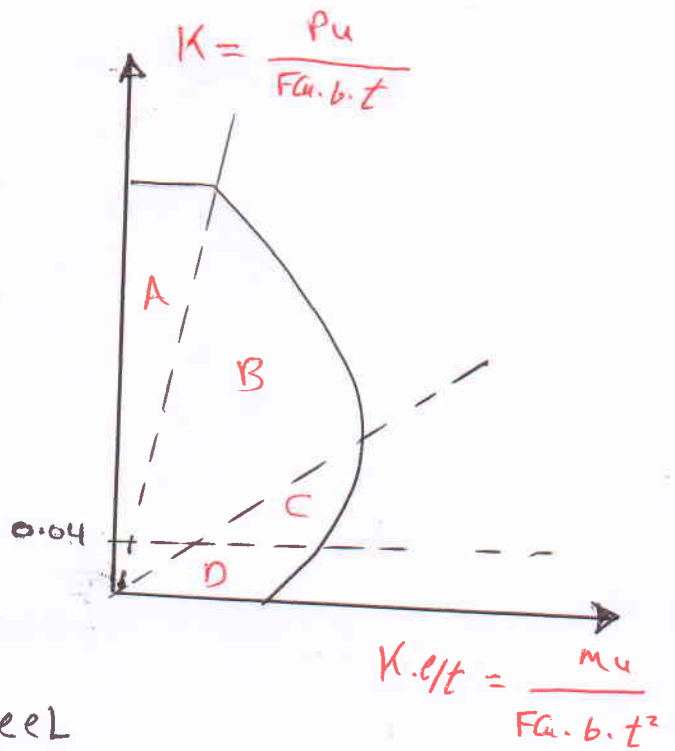
Zone B

$$\rho = 4$$

$$\lambda = \rho \times F_u \times 10^{-5} = 4 \times 250 \times 10^{-5} = 0.01$$

$$A_s = \lambda b t = 0.01 \times 25 \times 105 = 26.25 \text{ cm}^2$$

$$\text{Take } = 14 \phi 10$$





⇒ Check stirrups

$$V_s / V_c \geq 0.25\%$$

$$V_s = n * A_s * [\epsilon L] = 5 * 0.5 [8 * 20 + 2 * 100 + 57 * 2 + 32 * 2] = 39600 \text{ cm}^3$$

عدد الكائنات ←  
مساحة قطر الكائنات  
مجموع أطوال الكائنات الواحدة

$$V_c = 25 * 105 * 100 = 262500$$

$$\frac{39600}{262500} = 0.15 \geq \frac{0.25}{100} \quad \text{OK}$$

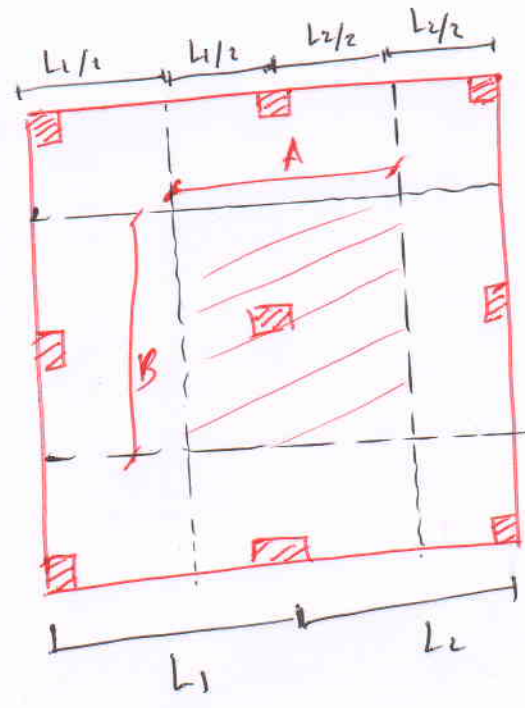
Area method

حساب مقدار الحديد (Pu) بطريقة

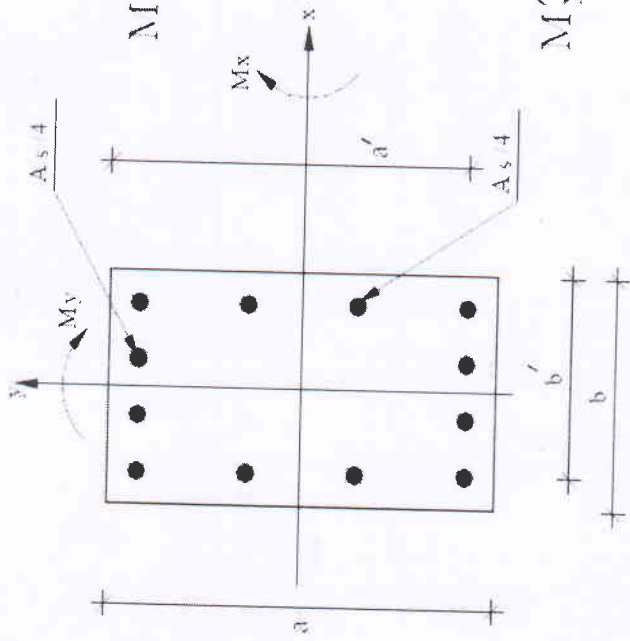
مجموع أطوال الكمرات في مساحة خدمة العوار  
 مجموع أطوال الجوانب في مساحة خدمة العوار

$$P_u = 1.2 \left[ 1.4 \left[ \rho_c \times t_s + F \cdot L + \frac{\rho_c \times b \times t_s \times \ell + \rho_w \times h_w \times t_w \times \ell}{A \times B} \right] + 1.6 \times L \cdot L \right] \times n \times A \times B$$

عدد الأتوار



# Design of Biaxial Column



$$M'_y = M_y + \beta \left( \frac{b'}{a'} \right) M_x$$

أ - في حالة  $\left( \frac{M'_x}{a'} \leq \frac{M'_y}{b'} \right)$

يؤخذ العزم التصميمي  $M'_y$  حول محور  $y$  طبقا للمعادلة

ب - في حالة  $\left( \frac{M'_x}{a'} > \frac{M'_y}{b'} \right)$

يؤخذ العزم التصميمي  $M'_x$  حول محور  $x$  طبقا للمعادلة

$$M'_x = M_x + \beta \left( \frac{a'}{b'} \right) M_y$$

\* ملحوظة يجب أن يكون  $\beta$  Diagonal  $\Rightarrow$  واحد  
 Inter ACTION Diagram  $\Leftrightarrow$

|  |         |      |      |      |         |
|--|---------|------|------|------|---------|
| $R_b = \frac{P_u}{f_{cu} \cdot b \cdot a}$ | $< 0.2$ | 0.3  | 0.4  | 0.5  | $> 0.6$ |
| $\beta$                                    | 0.80    | 0.75 | 0.70 | 0.65 | 0.60    |

$\Rightarrow P_u \& m_u$   
 $m_u$  or  $m'_x$   $\Rightarrow$  المنصف  $\Rightarrow$   $\Rightarrow$